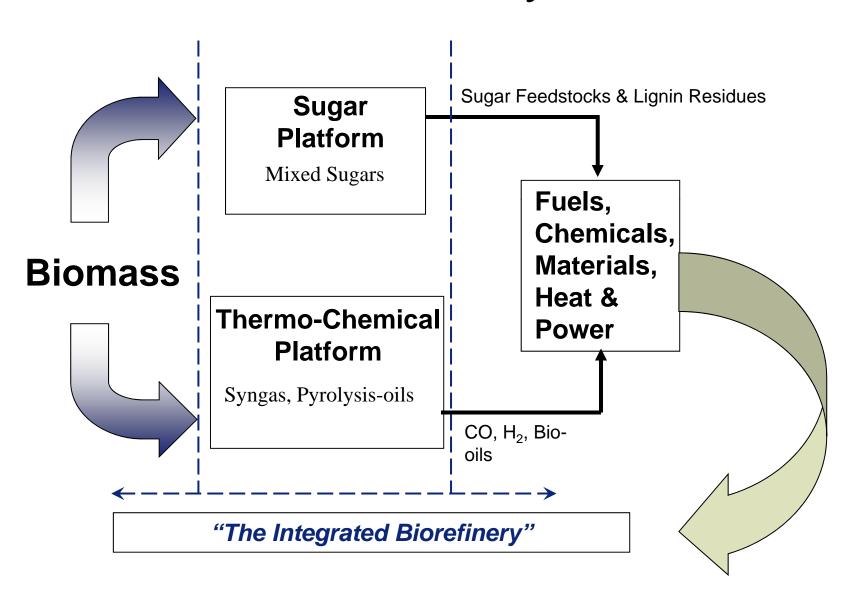
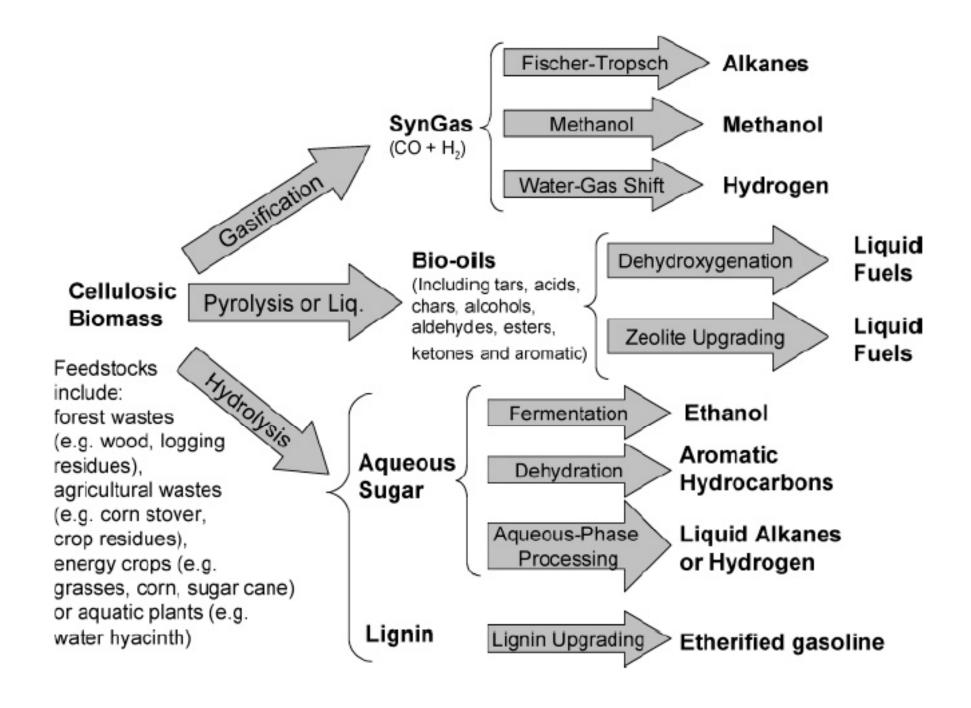
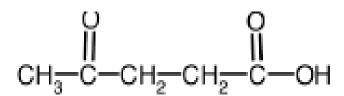
Biorefinery





Platform chemicals: cellulose

Levulinic acid





di Serena Fugalli Le Calorie Srl - Caserta. fugalliserena@msn.com

$$(C_6H_{10}O_5)_n + nH_2O \xrightarrow{[H^+]} n(C_6H_{12}O_6)$$

cellulosa + acqua → glucosio

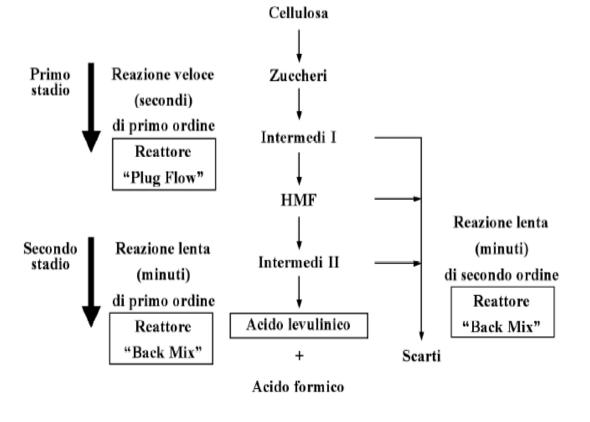
(in presenza di acido)

$$C_6H_{12}O_6 \xrightarrow{[H^+]} C_5H_8O_3 + HCOOH + H_2O$$

glucosio → acido levulinico + acido formico + acqua

Levulinic acid

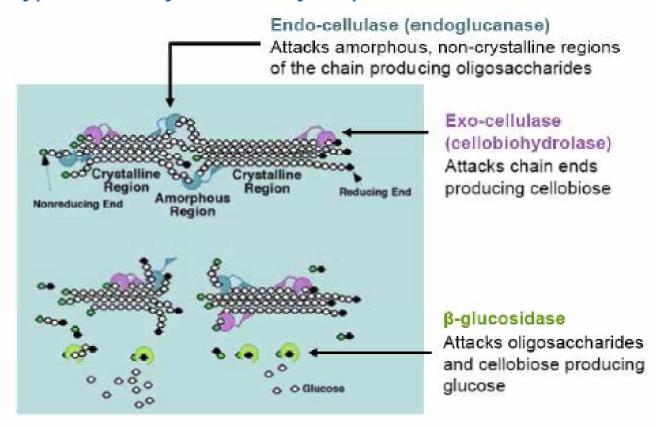




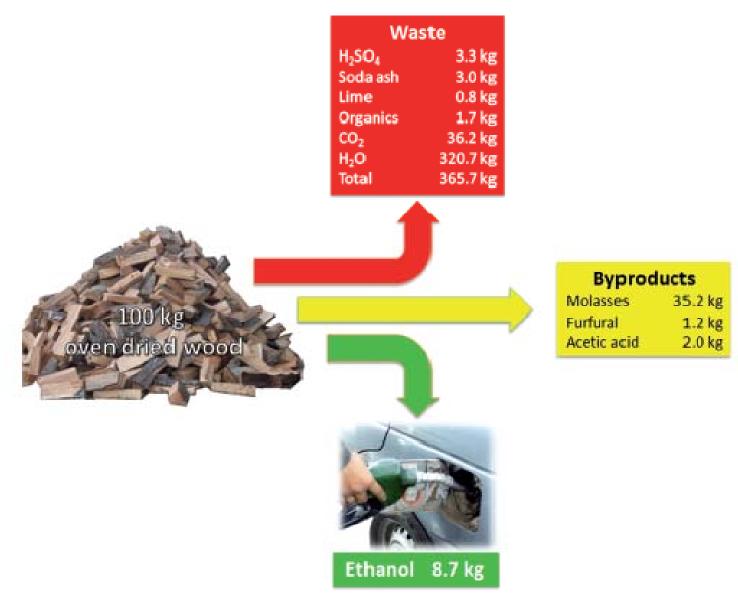
Hydrolysis reactor

Enzymatic cellulose hydrolysis

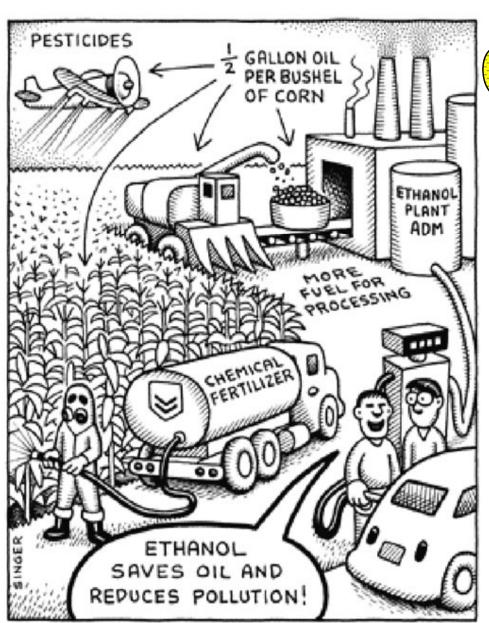
3 types of enzyme activity required



Source: Kevin A. Gray Ph. D., 2007. Conversion of lignocellulosic biomass into liquid transportation fuels Diversa Corporation/Celunol, San Diego, CA, USA. http://www.epobio.net/workshop0705/presentations/KevinGray.pdf

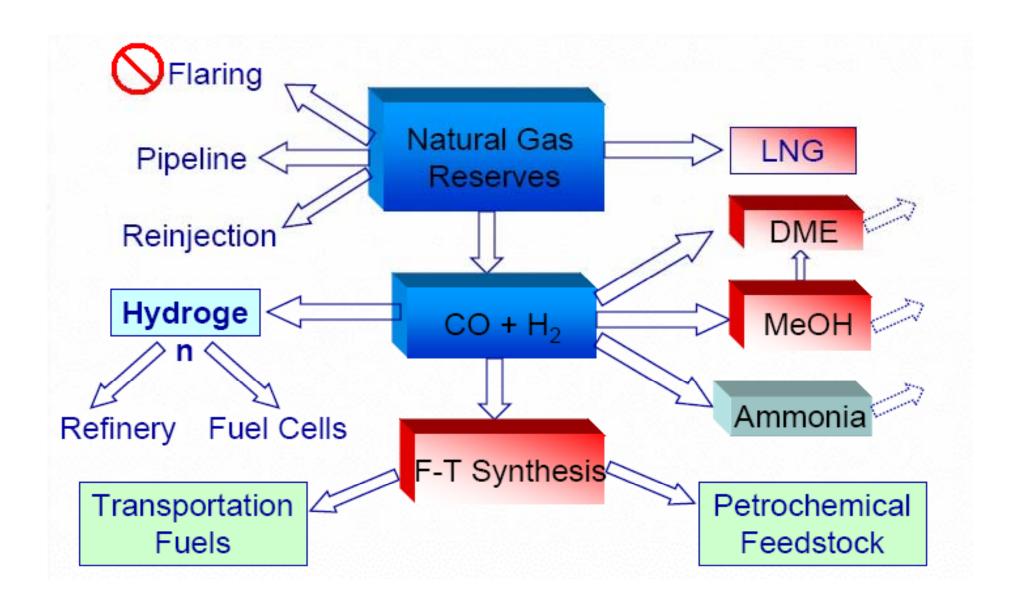


E-factor 40.2 kg waste per kg ethanol

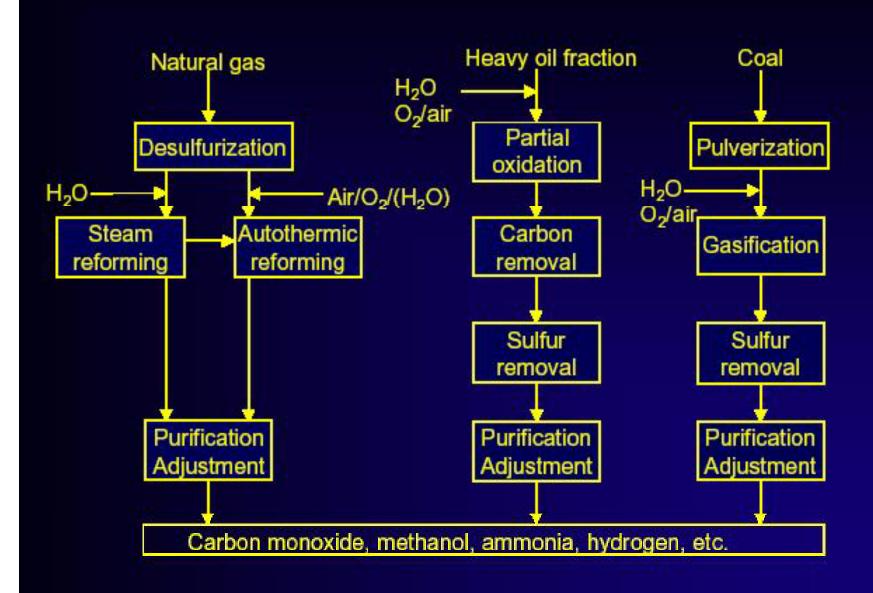


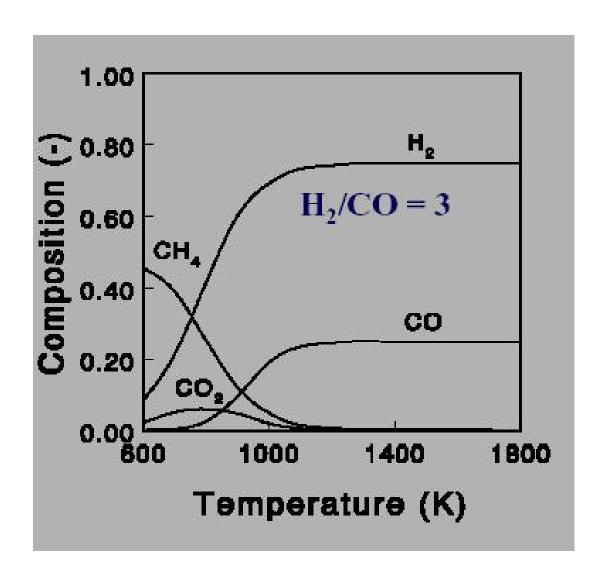
Corn vs Wood?

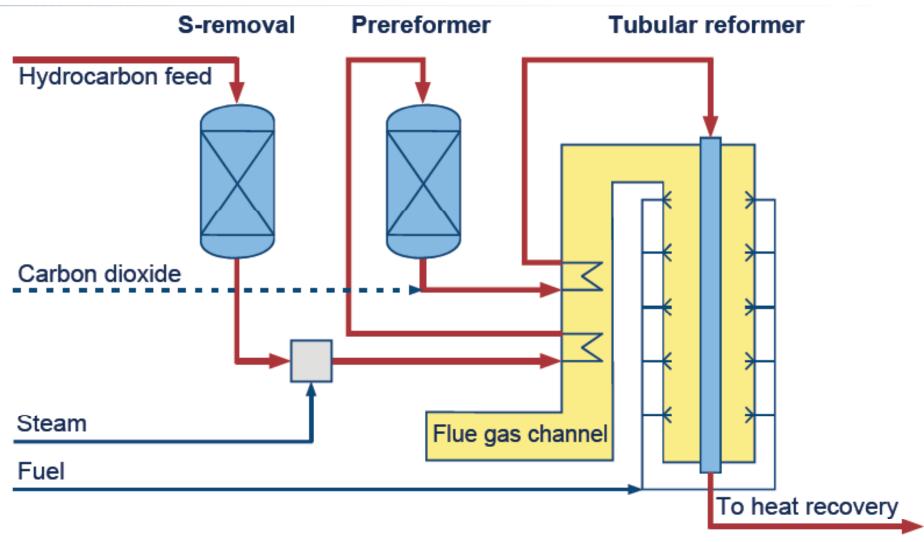




Conversion Routes to Synthesis Gas







- Adiabatic vessel with highly active nickel catalyst
- Converts higher hydrocarbons

Prereformer

- Allows higher preheat temperatures to tubular reformer or ATR
- Reduces size of tubular reformer
- Reduces oxygen consumption in ATR-based plant.

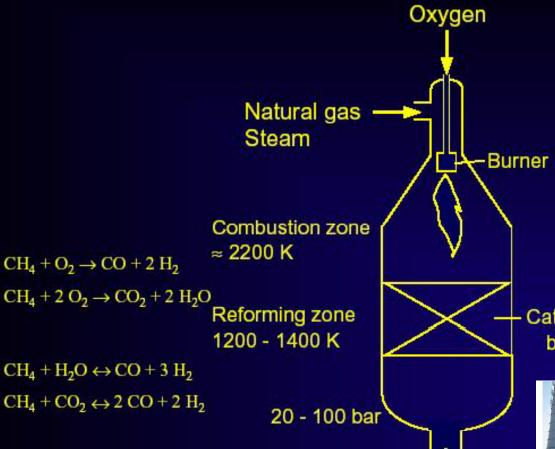






Tubes (500-600) filled with catalyst L=7-12 m, d=70-130 mm





Why O₂, not air?

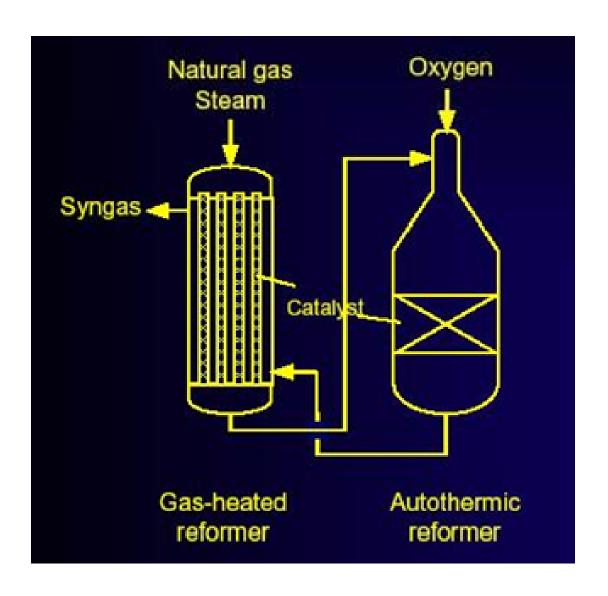
Molar feed ratio:

H₂O/CH₄: 1 - 2

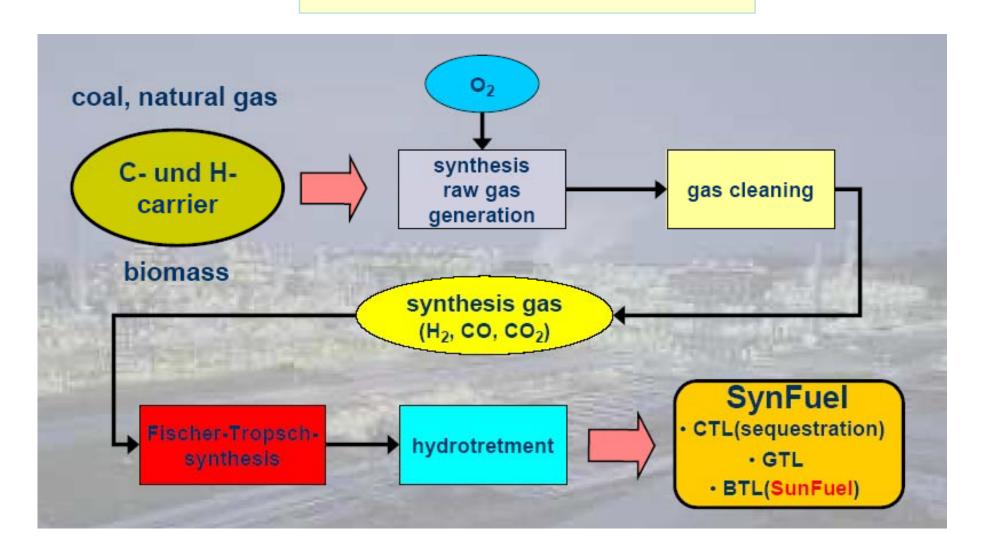
 O_2/CH_4 : ≈ 0.6

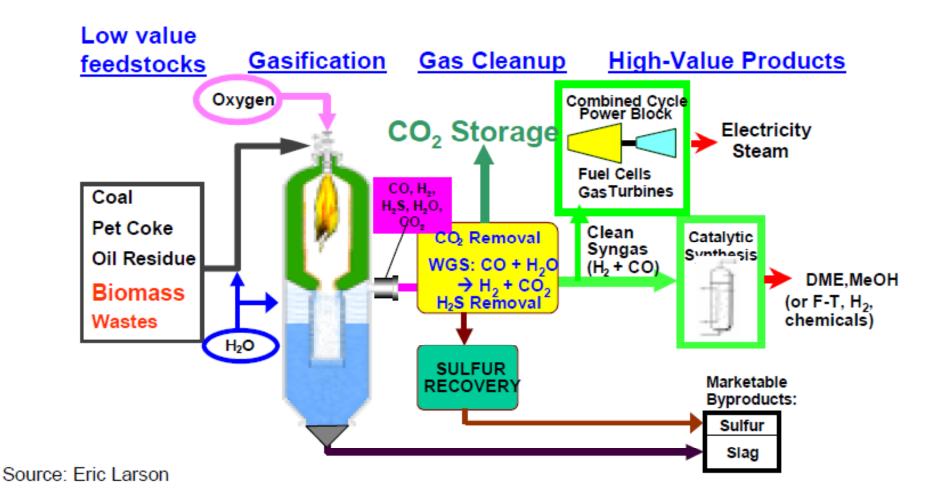
Catalyst bed





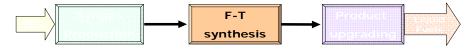
Gasification





→ Gasification is key technology for making clean fuels from coal or biomass and for low-cost CO₂ capture & storage

Fischer-Tropsch Reaction



$$nCO + 2nH_2 \rightarrow n(-CH_2-) + n H_2O \Delta H=-167 kJ/mole$$

CO + 3
$$H_2 \rightarrow CH_4 + H_2O$$
 Methanation ($\Delta H=-206$ kJ/mole)
CO + $H_2O \rightarrow CO_2 + H_2$ Water Gas Shift ($\Delta H=-41$ kJ/mole)
2CO \rightarrow C + CO_2 Boudouard reaction ($\Delta H=-172$ kJ/mole)
 $H_2 + CO \rightarrow C + H_2O$ Coke formation ($\Delta H=-133$ kJ/mole)

Main features of modern GTL-FT:

- Low temperature (200-240°C) and mid pressure (20-30 bar) to promote
 F-T over methanation reaction
- Active catalyst based on IRON or COBALT
- Production of high molecular weight linear waxes for further hydroprocessing step to optimize the overall liquid production, because it is impossible to produce directly a well defined range of products (i.e. middle distillates)

Fischer-Tropsch

Goal: production of liquid fuels or chemicals from gas

Also called: GTL

- political reasons (South Africa)
- remote gas fields (e.g., SMDS)

Main reactions

Alkanes $n \text{ CO} + (2n+1) \text{ H}_2 \rightarrow \text{ C}_n \text{ H}_{2n+2} + n \text{ H}_2 \text{ O}$

Alkenes $n \text{ CO} + 2n \text{ H}_2 \rightarrow \text{ C}_n \text{H}_{2n} + n \text{ H}_2 \text{O}$

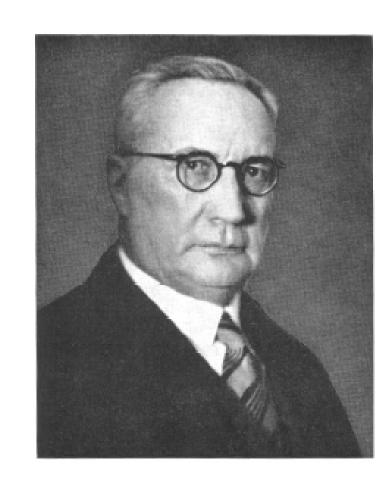
Water-gas shift $CO + H_2O \Rightarrow CO_2 + H_2$

Side reactions

Alcohols $n \text{ CO} + 2n \text{ H}_2 \rightarrow \text{H(-CH}_2\text{-})_n \text{OH} + (n\text{-}1) \text{ H}_2 \text{O}$

Bouldouard reaction $2 \text{ CO} \rightarrow \text{ C} + \text{ CO}_2$

Franz Fischer (1877-1947)



Professor Dr. Scanz Sischer, Geh. Reg.-Rat (Direktor des Instituts von der Gründung bis heute)

Hans Tropsch (1889-1935)



Dr.-Ing. Huns Tropfdy,
Rhteilungsvorfteher von 1921—1928
(am Inflitut tötig von 1915—1917 und 1921—1928)

CHEMISCHE WERKE ESSENER STEINKOHLE A.G., Bergkamen

Seprentanmeldung C 56 917

IV d/12 o vom 27. November 1941.

Verfahren zur Herstellung höherer Kohlenwasserstoffe durch katalytische Hydrierung von Oxyden des Kohlen-stoffs.

Basic F-T reaction

```
nCO + 2nH_2 \Rightarrow (-CH_2-)_n + nH_2O (\Delta H_R = -39.4 \text{ kcal/gmol}) [1]
```

- Stoichiometric H₂/CO ratio = 2
- Products predominantly normal paraffins, but may contain significant quantities of α-olefins and/or alcohols:

```
nCO + (2n+1)H_2 \Rightarrow C_nH_{2n+2} + nH_2O (n-paraffins)

nCO + 2nH_2 \Rightarrow C_nH_{2n} + nH_2O (\alpha-olefins)

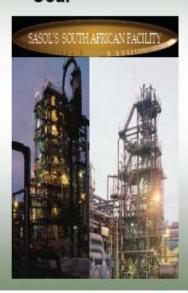
nCO + 2nH_2 \Rightarrow C_nH_{2n+1}OH + nH_2O (alcohols)
```

Fischer-Tropsch

- Hans Fischer and Franz Tropsch discovered the chemistry in 1923
- Germany commercialized the technology in WWII
- Today the future is bright

SASOL

- 160,000 b/d+
- Feedstock Coal



Petro SA

- · 22,500 b/d+
- Feedstock -Natural Gas



Shell

- · 15,000 b/d+
- Feedstock -Natural Gas

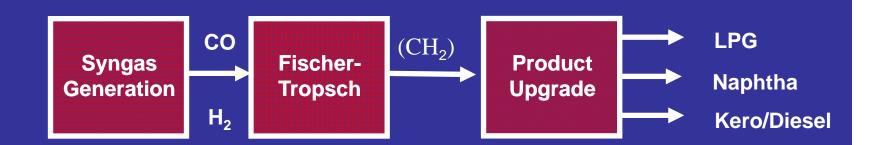


Sasol Oryx Project

- · 34,000 b/d
- Feedstock Natural Gas
- Online 2006



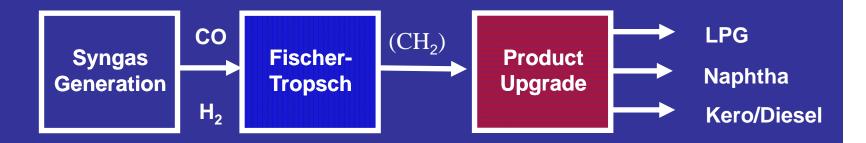
Gas-to-Liquids (FT) Process



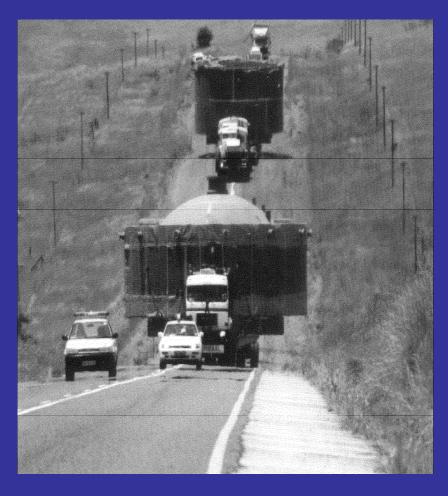
Technology – FT Process

Technical challenges

- Catalyst
- ·Heat removal
- Reactor design
- Scale-up



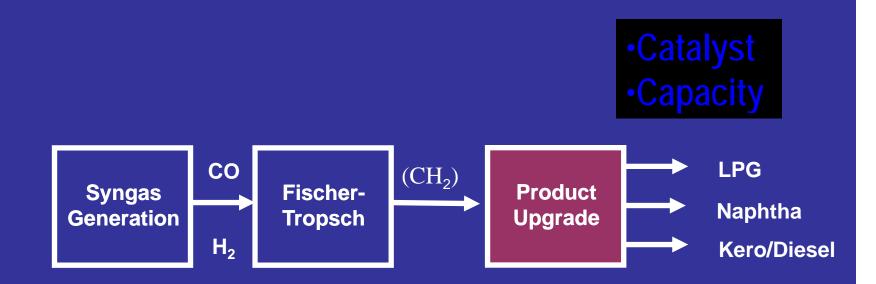
The Sasol Slurry Bed Reactor Technical challenges





Technical challenges

Technology - Product Upgrade



History

- 1902: Methane formed from H₂ and CO mixtures over Ni (Sabatier and Senderens);
- 1923: Fischer and Tropsch reported their work using Co, Fe, and Ru catalysts; at high pressure liquid hydrocarbon products formed over these catalysts;
- 1936: First four production plants commissioned in Germany (total capacity of 200,000 tons of hydrocarbons per year);
- 1944: Capacity of nine plants in Germany was increased to about 700,000 tons per year; Co based catalyst used in all production plants (development work on Fe catalysts continued but Fe not used to replace Co in production plant until after the 2nd WW);

History

- 1950: 5,000 bpd Hydrocol plant in Brownsville, Texas operated briefly (based on fixed fluid bed reactor, Fe-K catalyst, syngas from methane)
- 1950-53: Koelbel in Germany tested slurry phase F-T in pilot unit,1.5 m diameter (Rheinpreussen plant)
- 1950s Bureau of Mines plant in Louisiana, Missouri, operated briefly (Fe catalyst)
- Mid 1950's German plants were shut down after operating briefly on petroleum residue. Interest in F-T synthesis declined worldwide with the discovery of abundant oil deposits in the Middle East.
- Except in South Africa where the first Sasol plant (Sasol I)was commissioned in 1955 (Based on Fe catalyst, Arge fixed bed and circulating fluid bed reactors); These were followed by Sasol II (1980) and Sasol III (1983), based on Synthol circulating fluid bed technology

NOVOCHERKASSK SYNTHETIC PRODUCTS PLANT 1954-1992

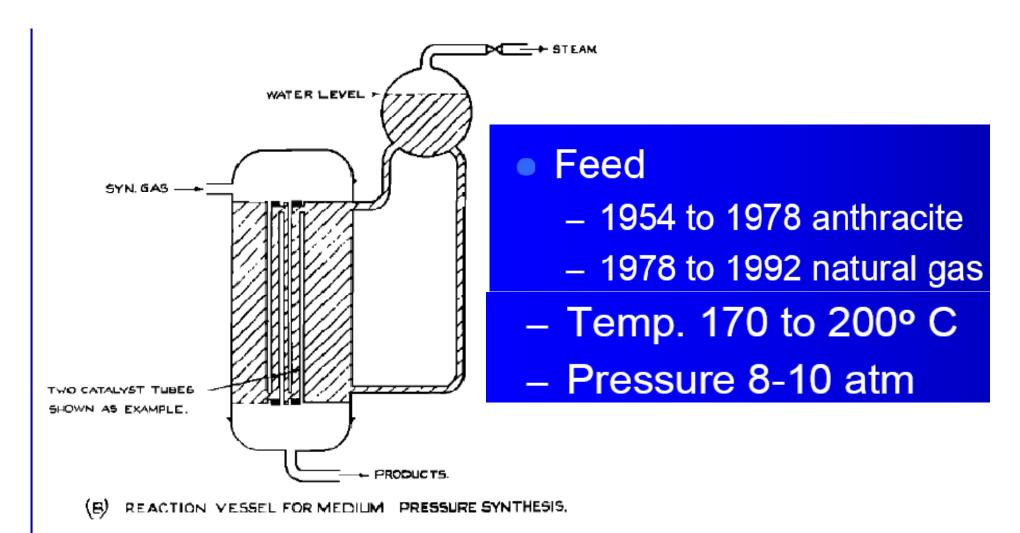
Design FT Plant

- Planned capacity 50,000 tpy
- Primary commercial products
 - n-paraffins(C₅-C₂₄ reference cetane)
 - solvents (C₅-C₆ and C₆-C₇ paraffin fractions)
 - Oxidation feedstocks (paraffin fractions 179-270, 260-290°C)
 - solid paraffins (ceresin)

Disadvantages

- Low process productivity
 - 4 t catalyst reactor load produces 2.5 t/day of C₂₊
- Uneconomical production
- Co catalyst is no more than 9-12 months.

Novocherkassk



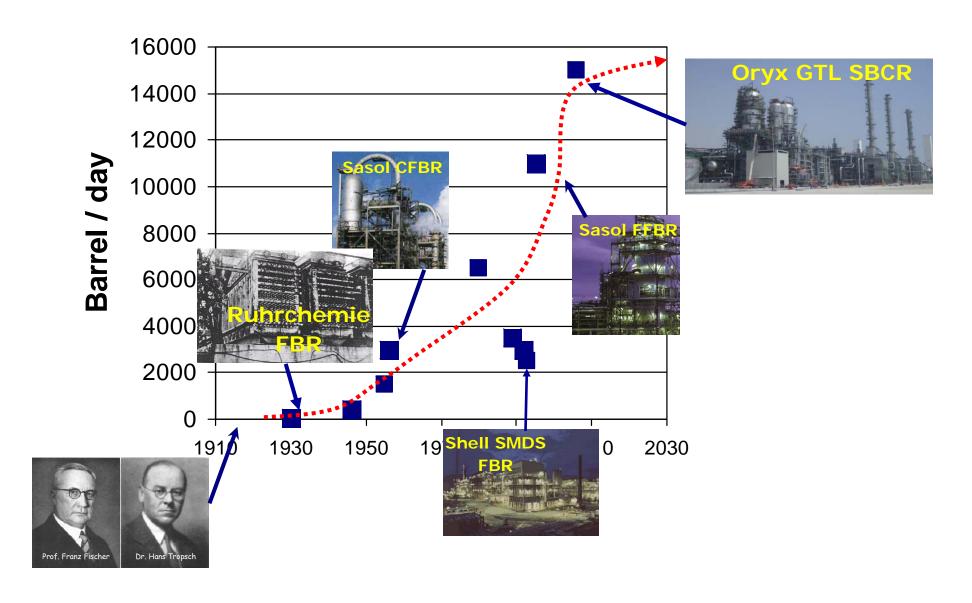
Novocherkassk

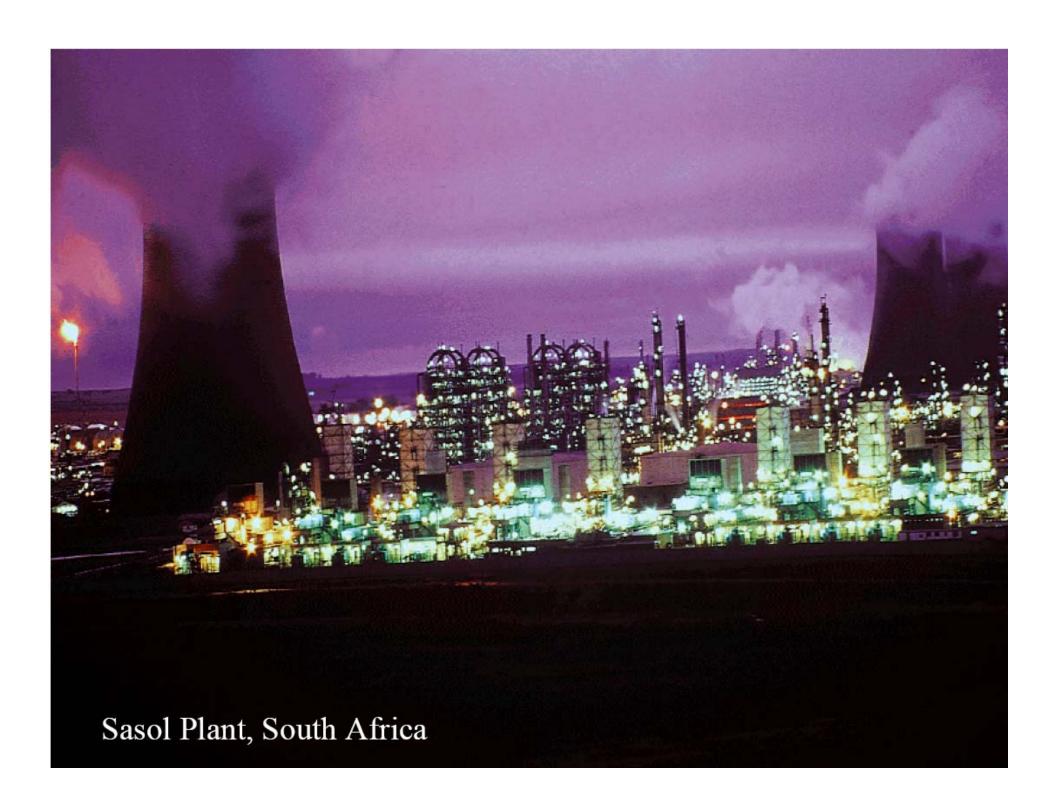
- 1954- 1967 German Formulation
 - 100 Co, 8 MgO, 5 ThO₂, 200 kieselgur
- 1967 1977 Thoria Free Catalyst
 - 200 Co, 10 MgO, 260-280 kieselgur
- 1977 1981 Ceresin yield improvement
 - 100 Co, 10 ZrO₂, 200 kieselgur
- 1981-1992 Ceresin yield improvement
 - 100 Co, 10 MgO, 10 ZrO₂, 200 amorphous synthetic aluminosilicate

History

- 1970's and 1980's renewed interest in F-T synthesis due to increasing oil prices and fear of oil shortage
- 1990's further revival of F-T or GTL due to discoveries of huge "stranded" natural gas reserves, and requirements for cleaner fuels
- 1992: Mossgas large plant using Sasol technology and syngas from natural gas
- 1992-1993: Startup of Shell middle distillate 13 000 bbl/d plant in Malaysia (fixed bed reactor, Co catalyst and syngas from natural gas)
- 1993 Sasol slurry phase 2500 bbl/d F-T reactor (Fe catalyst)

FT Reactor Capacities Historical overview



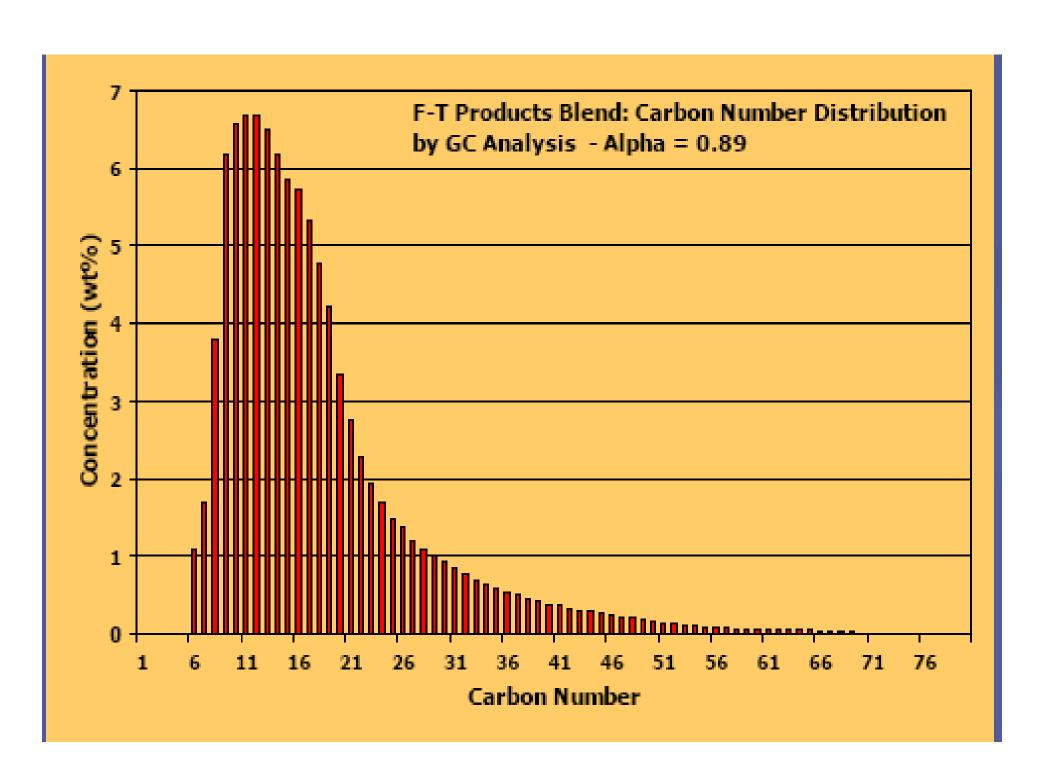


Mechanism

- Exact mechanism very complex, not well defined, and still the subject of much debate
- F-T mechanism may be divided into at least 3 major steps:
 - Initiation or C₁ compound formation by:
 - CO adsorption on catalyst metal surface
 - C O bond breakage
 - Hydrogenation of *C to *CH₂
 - 2. Hydrocarbon chain growth by;
 - Successive insertion of the C₁ building blocks
 - 3. Chain termination by:
 - Desorption of unsaturated surface species
 - Hydrogenation and desorption of saturated species

Products

- Product composition strongly influenced by
 - Catalyst composition
 - Product from cobalt catalyst higher in paraffins
 - Product from iron catalyst higher in olefins and oxygenates
 - Operating conditions
 - Temperature
 - Pressure
 - H₂/CO ratio
- However, essentially no aromatics except for high temperature processes, no nitrogen or sulfur compounds



- F-T chemistry can be viewed as a polymerization reaction
- Applying polymerization kinetics, a simple oneparameter equation can describe the entire product distribution, referred to as the Anderson-Shultz-Flory (A-S-F) distribution:

$$W_n = (1-\alpha)^2 n \alpha^{n-1}$$

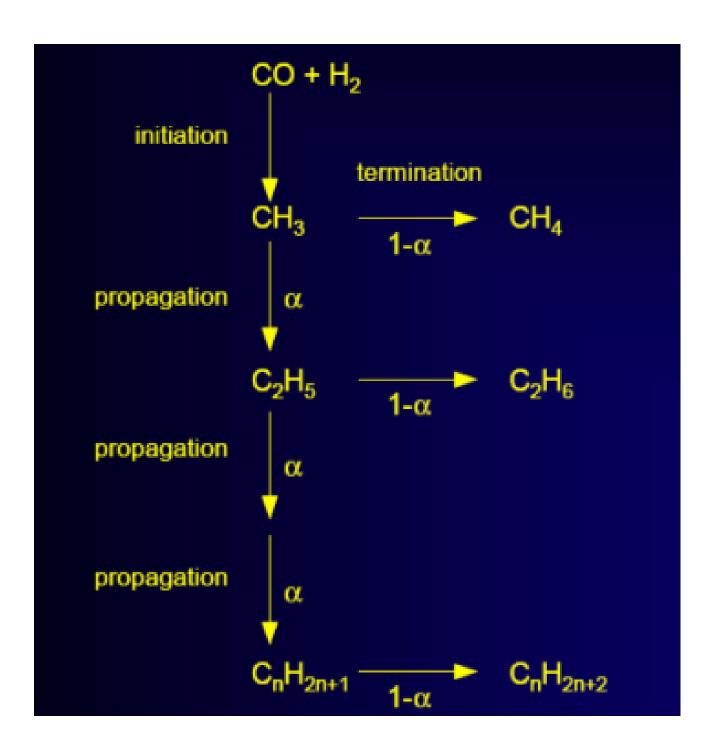
where:

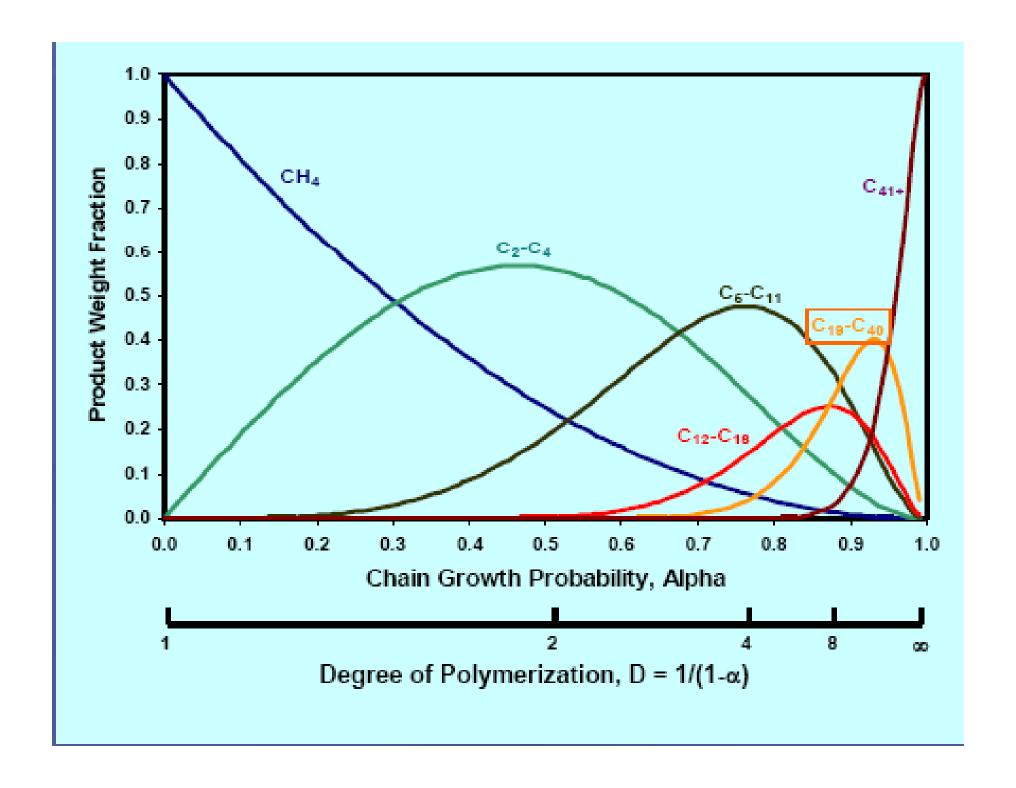
n = carbon number

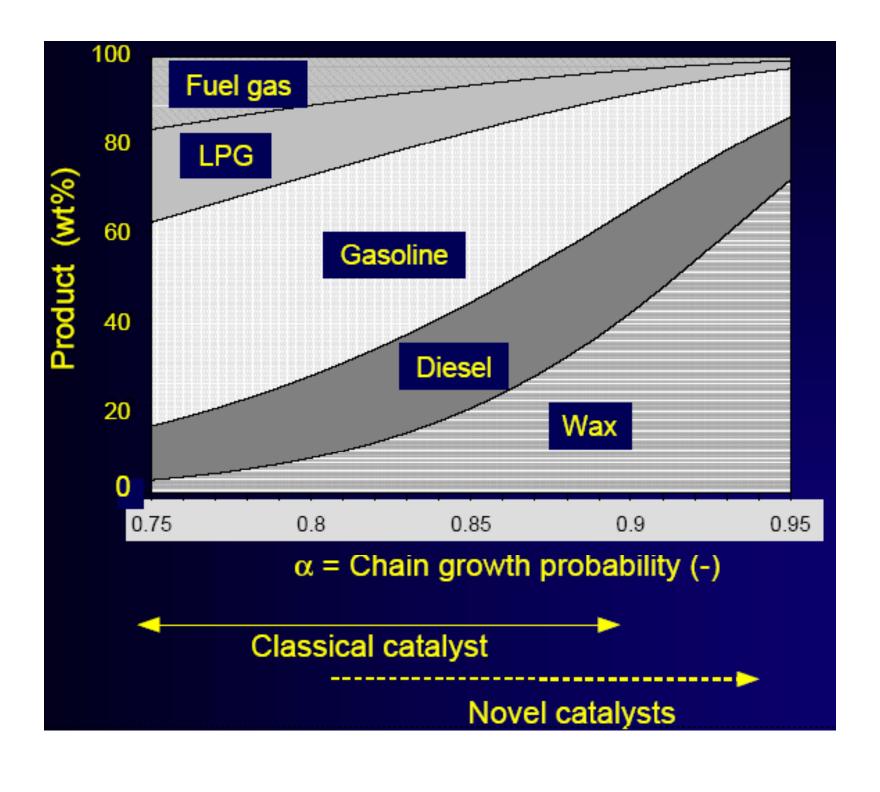
W_n = Weight fraction of product with carbon number n

 α = Chain growth probability

 The higher the value of α the longer the average chain length







Kinetics

F-T chemistry often modeled by a simple power law equation:

$$-r_{CO} = Ae^{-E/RT} p_{H2}^{m} p_{CO}^{n}$$

where:

```
r<sub>CO</sub> = rate of conversion of CO
p<sub>H2</sub>, p<sub>CO</sub> = partial pressure of H<sub>2</sub> and CO, respectively
```

- In general m is positive (~ 1.0) and n is negative (-0.1 - -0.35)
- Energy of activation generally found in the range of 20 –25 kcal/gmol

Catalysts

SOURCE OF CARBON	F-T CATALYST	QUALIFICATIONS	
Any	Ni	methanation	
Carbon-rich [coal]	Fe	WGS activity with CO ₂ production	
Hydrogen-rich [natural gas]	Со	Very active, linear hydrocarbons	
	Ru	Very active, VERY EXPENSIVE!	

Catalysts

- F-T Active Metal (Co, Fe, Ru)
- Reduction Promoters (Pt, Ru, Pd, Re, Cu)
- Activity/Selectivity Promoters (K, Zr, RE, etc.)
- Refractory oxide (Al₂O₃, SiO₂, TiO₂) used as supports or structural promoters

Fe

- Catalyst that has received most studies
- Used commercially in S. African F-T plant
- Generally preferred for coal-based syngas (low H₂/CO ratio)
- Can be prepared in several ways:
 - Fused iron oxide (used inn Sasol's Synthol reactors); promoters added in the fusion step; much cheaper to prepare
 - Sintered iron oxide
 - Precipitated iron oxide which permits coprecipitation of additives and modifiers; however, more expensive to produce and has less structural strength
- Inherently unstable and gradually loose activity;
 cannot be regenerated; must be replaced periodically
- Structurally unstable for slurry reactor applications
- Typically promoted with copper to improve reducibility of Fe and an alkali (preferably K)

Co

- Generally preferred for natural gas-based syngas which is provided at close to or higher than F-T stoichiometric H₂/CO ratio
- Its low WGS activity, an advantage for such syngas.
- Earlier Co catalysts prepared by coprecipitation methods
- New generation of Co catalysts prepared mostly by impregnation of oxide supports, using aqueous or organic solutions of Co nitrates and other additives
- Nitrates easily decomposed by calcination
- Co oxide usually pre-reduced in a H₂ containing gas to convert it to a metal active state
- Co catalyst currently used commercially in Shell F-T plant in Malaysia, and the catalyst of choice in most if not all future F-T plants based on natural gas feedstock



Cobalt Particle Size Effects in the Fischer—Tropsch Reaction Studied with Carbon Nanofiber Supported Catalysts

G. Leendert Bezemer,[†] Johannes H. Bitter,[†] Herman P. C. E. Kuipers,[‡] Heiko Oosterbeek,[‡] Johannes E. Holewijn,[‡] Xiaoding Xu,[§] Freek Kapteijn,[§] A. Jos van Dillen,[†] and Krijn P. de Jong*,[†]

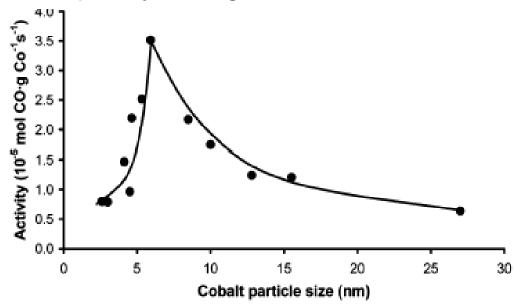


Figure 7. The influence of cobalt particle size on activity normalized to the cobalt loading (220 °C, $H_2/CO = 2$, 1 bar).

J. AM. CHEM. SOC. 2006, 128, 3956

Co catalysts

- Support (Al₂O₃, SiO₂, TiO₂)
 - High surface area adsorbent
 - Adequate particle size distribution
 - Chemically and physically stable in environment of:
 - Catalyst preparation
 - Catalyst activation/regeneration
 - F-T reaction

Active Metal

- Cobalt chemically activates sorbed CO and enables its hydrogenation
- Uniformly distributed on support
- Active only in metallic form
- Stable in synthesis environment

Co catalysts

- Oxide promoters (from groups IA, IIA, IIIA, IVA or VA of the periodic table)
 - Stabilize the dispersion of cobalt on catalyst surface
 - Promote hydrocarbon chain growth
 - Limit cobalt-support compound formation

- Noble metal promoters (Pt group metals)
 - Facilitate reduction of cobalt oxide to metal during:
 - Catalyst activation
 - Catalyst regeneration

Summary: FT Catalyst

Active Phase: Cobalt, Iron

Co based catalyst

- Expensive
- High selectivity to long chain paraffins
- Low selectivity to olefins and oxygenates
- resistant to deactivation
- limited WGS activity

Fe based catalyst

- → Economic
- Low selectivity to long chain paraffins
- High selectivity to olefins and oxygenates
- → WGS catalyst
- → Fast deactivation (coke)

♣ Promoter

- → Structural: increase metal dispersion (Re, Zr, Hf, Ce)
- → Reduction: increase extent of reduction (Ru, Pd, Pt, Cu)
- Activity: prevent coke deposition (Noble Metals)
- Selectivity: alter the product distribution (Na, K, Cs)

♣ Carrier: SiO₂, Al₂O₃, TiO₂, mix

- Structural promoter itself
- → Influence selectivity due to secondary reaction (i.e. acid sites)

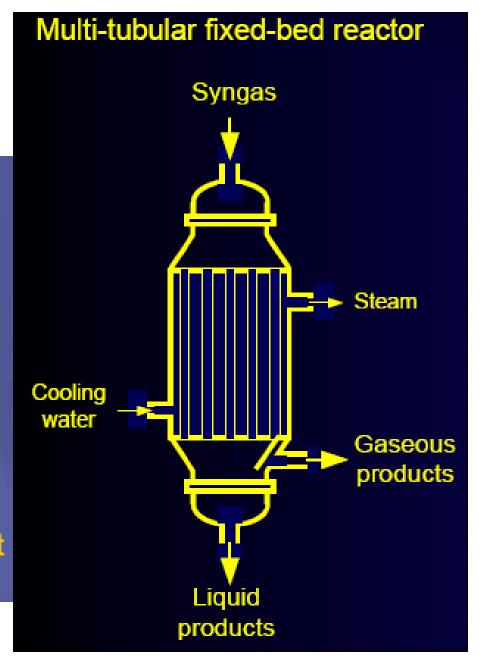
Catalysts

	Typical Catalyst Constituents			
Company	Primary	Reduction Activity/Selectivity Promoter Promoter		Support
Conoco	Co	Re, other	N/A	Alumina, other
Gulf (Shell)	Co	Ru	oxide promoters	alumina
Exxon	Co	Re/Ru	oxide promoters	titania or TiO ₂ /silica
IFP	Co			
Intevep	Co	-	oxide and carbide promoters	Silica
Rentech	Fe	N/A	N/A	-
Shell	Co	with or w/o a noble metal	ZrO ₂	Silica, silica- alumina
Statoil	Co	Re	oxide promoters	alumina
SASOL	(Fe) Co	Pt	-	alumina
Williams	Co	with or w/o a noble metal	with or w/o oxide promoters	doped alumina

Reactors

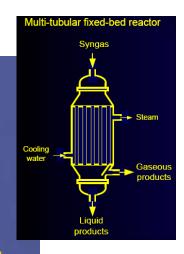
- F-T reaction is highly exothermic
- Heat removal is a major consideration when designing a F-T reactor
- Selectivity to methane increases with increasing temperature
- Close temperature control necessary in order to maintain desired selectivity
- Three major types of reactors are considered for F-T process:
 - Tubular fixed bed reactor
 - Fluidized bed reactor
 - Slurry reactor

- First reactor type to be exploited commercially, e.g., Arge reactor
- TFB reactors used in Sasol I in South Africa and Shell plant in Malaysia
- Catalyst in pellet shape are placed in the tubes and the cooling medium flows around the outside of the tubes, similar to a shell and tube heat exchanger



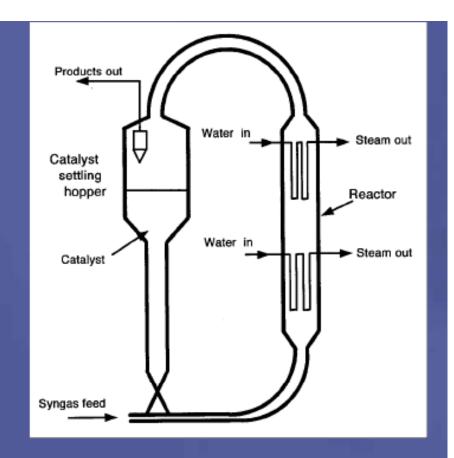
Fixed bed

- Relatively simple design, but expensive construction with its large number of tubes required for a commercial scale plant
- Easy to scale-up from a single tube pilot plant
- Catalyst replacement is a major undertaking
- Iron catalysts inherently unstable have to be replaced periodically
- More stable cobalt catalysts can be regenerated and reactivated in-situ; may not have to be replaced for several year
- May experience temperature gradients in the tubes which can lead to catalyst sintering and deactivation
- Can also experience high pressure drop in tubes



Reactors

- Two types of FB reactors:
 - Circulating fluidized bed (CFB) reactor such as the Sasol's Synthol reactor
 - Fixed fluidized bed reactor (Sasol Advanced Synthol, SAS reactor)
- CFB reactors used in Sasol I and II
- Better heat removal
- Better temperature control
- Less pressure drop problems
- Online catalyst removal and addition possible



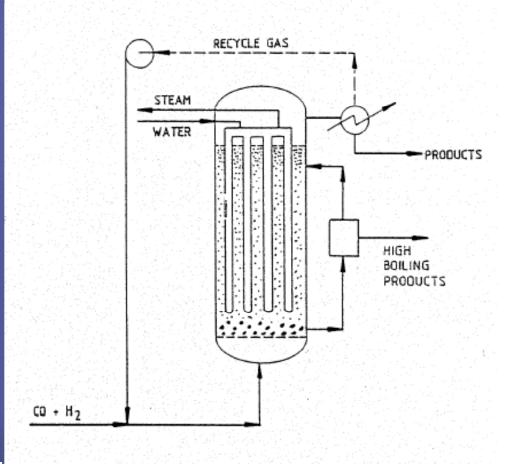
Sasol's (Synthol) Circulating Fluidized Bed Reactor

Fluidized beds

- Major disadvantage of fluidized beds for F-T applications: Product must be volatile at the reaction conditions
- Non-volatile hydrocarbons can accumulate on catalyst particles, making them sticky and adhering to each other; the bed looses its fluidization properties
- Thus, the F-T products of fluidized bed reactors must be of relatively low molecular weight
- More difficult to scale-up than TBF reactors, because the fluidization behavior function of the reactor diameter
- However, there is a wide experience with large fluidized bed reactors in refining, such as FCC units; thus fluidized bed reactors can be scaled-up with confidence

Slurry

The slurry-phase bubble column reactor (SBCR) considered the primary choice for the newer F-T processes using highly active cobalt catalysts In a SBCR syngas is bubbled up through a slurry made up of hydrocarbon wax, liquid at the reaction conditions, and a catalyst suspended in it The catalyst is a finely divided powder with an average particle size of 50-80 μm



Slurry

- Advantages provided by the use of SBCR:
 - Good heat transfer
 - Excellent temperature control
 - Better selectivity control
 - Ideal for higher boiling products
 - Low pressure drop
 - Ease of adding and removing catalyst
 - Simple design and construction
 - Potentially high capacity (10000-20000 bbl/d)
- The gaseous products are removed from the top of the reactor, while the heavy non-volatile wax must be separated from the catalyst which remains in the reactor
- Various proprietary internal or external filtration systems have been devised

Operation

- Operating conditions influenced by reactor type as well as the nature of the catalyst
- Main controlling parameters:
 - Temperature: 220-350 °C for iron; 200-250 °C for cobalt; high temperature required for fluidized bed reactors
 - Pressure: atmospheric 500 psi
 - Space velocity: 100-1000 h⁻¹
 - H₂/CO ratio depends on the source of syngas and type of catalyst
 - Optimum per pass conversion may be more of an economical decision than a technical one

Reactor comparison

	Multi-tubular fixed- bed reactor	Riser reactor	Slurry reactor
Conditions			
Inlet T (K)	496	593	533
Outlet T (K)	509	598	538
Pressure (bar)	25	23	15
H ₂ /CO feed ratio	1.7	2.54	0.68*
Conversion (%)	60 – 66	85	87
Products (wt%)			
CH ₄	2.0	10.0	6.8
C_2H_4	0.1	4.0	1.6
C_2H_6	1.8	4.0	2.8
C_3H_6	2.7	12.0	7.5
C_3H_8	1.7	1.7	1.8
C_4H_8	2.8	9.4	6.2
C_4H_{10}	1.7	1.9	1.8
C ₅ – C ₁₁ (gasoline)	18.0	40.0	18.6
$C_{12} - C_{18}$ (diesel)	14.0	7.0	14.3
C_{19}^+ (waxes)	52.0	4.0	37.6
Oxygenates	3.2	6.0	1.0

Technologies

In use/Ready to go

Company	Reactor	Catalyst
Shell SMDS	FB	Со
SASOL SPD	SBCR	Со
Exxon AGC-21	SBCR	Со
Rentech	SBCR	Fe
Syntroleum	FB	Со

Plants

EXISTING PLANTS					
Owner	Location	Products	Capacity,b/d	Feedstock	Start date
SASOL I	Sasolburg	Fuels/Specialty	2,500	Coal	1955
SASOL II	Secunda	Fuels/Specialty	85,000	Coal	1980
SASOL III	Secunda	Fuels/Specialty	85,000	Coal	1982
NZ Synfuels	New Plymouth	Fuels	12,000	Natural Gas	1985
Shell	Bintulu	Fuels/Specialty	12,500	Natural Gas	1993
MossGass	Mossel Bay	Fuels/Specialty	30,000	Natural Gas	1992
	Pi	LANNED COMME	ERCIAL PLANT	's	
Owner	Location	Products	Capacity,b/d	Feedstock	Start date
Exxon/Mobil	Qatar	Fuels	80,000	Natural Gas	2005
Sasol/Qatar	Qatar	Fuels	34,000	Natural Gas	2005
Chevron	Nigeria	Fuels/Specialty	34,000	Natural Gas	2005
Syntroleum	Australia	Specialty	11,500	Natural Gas	2005

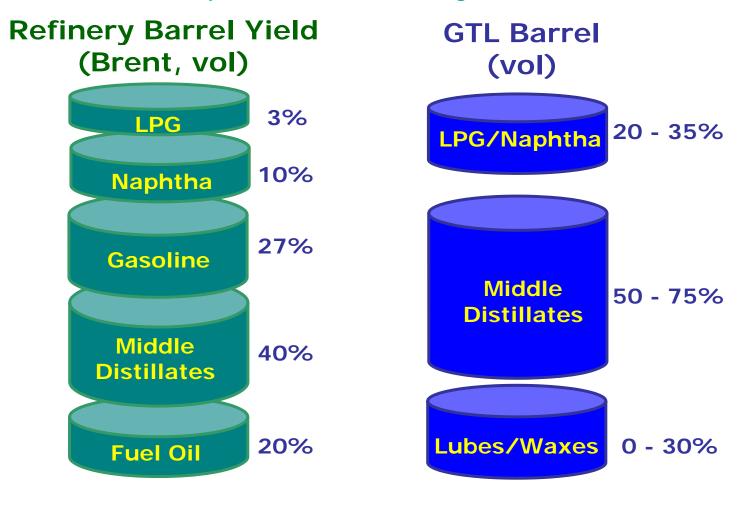
Table 1 Fischer–Tropsch processes currently in industrial operation

Type	FT catalyst	FT reactor type	FT technology	Operator	Commercial operation	
HTFT HTFT LTFT LTFT LTFT LTFT	fused Fe fused Fe precipitated Fe precipitated Fe Co-SiO ₂ Co-Al ₂ O ₃	circulating fluidised bed fixed fluidised bed fixed bed slurry bubble column fixed bed slurry bubble column	Sasol Synthol Sasol Advanced Synthol (SAS) ARGE ^a Sasol Slurry Bed Process (SSBP) Shell Middle Distillate Synthesis (SMDS) Sasol Slurry Bed Process (SSBP)	PetroSA Sasol Sasol Sasol Shell Sasol	Mossel Bay, South Africa Secunda, South Africa Sasolburg, South Africa Sasolburg, South Africa Bintulu, Malaysia Ras Laffan, Qatar	
^a ARGE = Arbeitsgemeinschaft Ruhrchemie-Lurgi.						

Products from GTL-FT process

Typical FT product composition after upgrading is: 25% Virgin Naphtha, 25% Jet Fuel and 50% Diesel

and minor amounts of LPG and bottom hydrocracking. The heavier fraction can be used for the production of lubricating bases or chemicals.



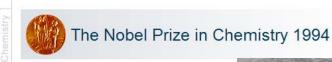
GtL Technology: Hydrocraking

Conventional vs. GtL Diesel

Quality	Convention al Diesel	SWCL1	Blu Diesel Agip	FT – Diesel #
Boiling range (°C)	180-360	180-275	180-360	150-360
Density @ 15°C (kg/m³)	820 — 845	805	835	780
Sulfur (ppm vol)	50	6	4.5	<1
Aromatics (% vol)	30	3	22	< 0.1
Cetane number (CN)	> 51	56	55	> 70
CFPP* (°C)	- 15	- 12	- 11	-20
Cloud point (°C)	0	n.d.	-1	-15

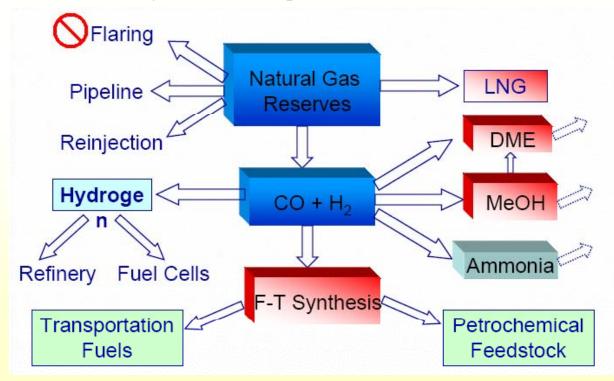
^{*} Cold Filter Plug Point;

[#] Diesel from waxes produced on pilot runs



G.Olah: Beyond Oil and Gas: The Methanol Economy

- storing energy in the form of methanol
 - excellent fuel; easily stored, transported and used





Methanol

$$CO+2H_2$$
 \longrightarrow CH_3OH , $\Delta H=-90.8 \text{ kJ/mol}$

$$CO_2+3H_2$$
 CH_3OH+H_2O , $\Delta H=-49.6$ kJ/mol

$$CO+H_2O$$
 \longrightarrow CO_2+H_2 , $\Delta H=-41 \text{ kJ/mol}$

T low

By-products: higher alcohols and hydrocarbons from CO

Phase: gas

Catalyst: selective CuZn/Al₂O₃

Methanol

Catalyst: sintering possible, thus t< 200-270°C deactivation by S, C⇒(purification)

Operation policy: pressure increase with deactivation (not T)

Gas composition: 74% H_2 , 15% CO, 8% CO_2 , 3% CH_4 p=50-100 bar, conversion 15-30% in adiabatic reactor

Recycle of gases : recycle/make-up = 3-7 (range to avoid build up of CH_4 and Ar)

Products: distillation

Improvements: 1) remove heat to keep reaction T as low as possible

2)removal of methanol to shift equilibrium

3) more active catalyst

Mechanism of methanol formation

MECHANISM A

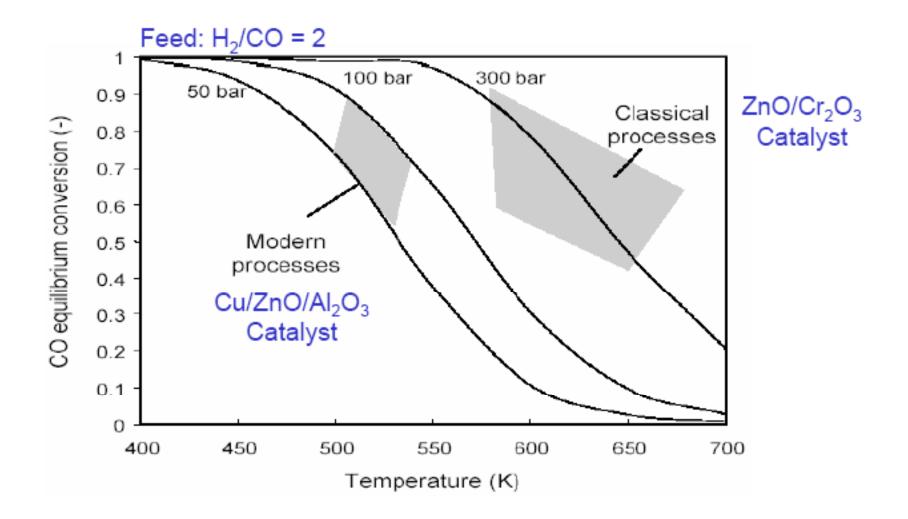
MECHANISM B

$$CO \longrightarrow \overset{CO}{*} \longrightarrow \overset{H}{*} \longrightarrow \overset{C}{*} \longrightarrow \overset{H}{*} \longrightarrow \overset{CH_2OH}{*} \longrightarrow \overset{H}{*} \longrightarrow \overset{CH_2OH}{*} \longrightarrow \overset{H}{*} \longrightarrow \overset{CH_3OH}{*} \longrightarrow \overset{C$$

Methanol synthesis mechanism

$$H_2O(g) + * \rightleftharpoons H_2O*$$
 $H_2O* + * \rightleftharpoons OH* + H*$
 $2OH* \rightleftharpoons H_2O* + O*$
 $OH* + * \rightleftharpoons O* + H*$
 $2H* \rightleftharpoons H_2(g) + 2*$
 $CO(g) + * \rightleftharpoons CO*$
 $CO* + O* \rightleftharpoons CO_2* + *$
 $CO_2* \rightleftharpoons CO_2(g) + *$
 $CO_2* + H* \rightleftharpoons HCOO* + *$
 $HCOO* + H* \rightleftharpoons H_2COO* + *$
 $H_2COO* + H* \rightleftharpoons H_3CO* + O*$
 $H_3CO* + H* \rightleftharpoons CH_3OH* + *$
 $CH_3OH* \rightleftharpoons CH_3OH(g) + *,$

Rate determining step



Methanol

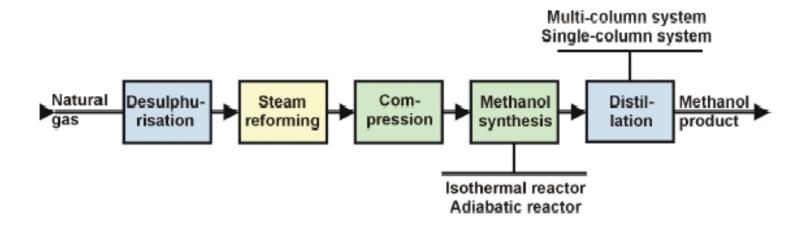
Table 6.10 Equilibrium CO and CO₂ conversions, and exit CH₃OH concentration versus pressure and temperature³ for methanol synthesis (Wade et al., 1981)

Temperature (°C)	CO conversion (%)			CO ₂ conversion (%)			Exit CH ₂ OH (vol %)		
	50 bar ^b	100 bar	300 bar	50 bar	100 bar	300 bar	50 bar	100 bar	300 bar
200	95.6	99.0	99.9	44.1	82.5	99.0	27.8	37.6	42.3
250	72.1	90.9	98.9	18.0	46.2	91.0	16.2	26.5	39.7
300	25.7	60.6	92.8	14.3	24.6	71.1	5.6	14.2	32.2
350	-2.3	16.9	73.0	19.8	23.6	52.1	1.3	4.8	21.7
400	-12.8	-7.2	38.1	27.9	30.1	44.2	0.3	1.4	11.4

^{*} Typical reformed natural gas composition 15% CO, 8% CO₂, 74% H₂, 3% CH₄; H₂/(2CO + 3CO₂) = 1.30; simplified single-pass operation, no recycle.

h 1 bar = 1.013 atm.

Methanol synthesis



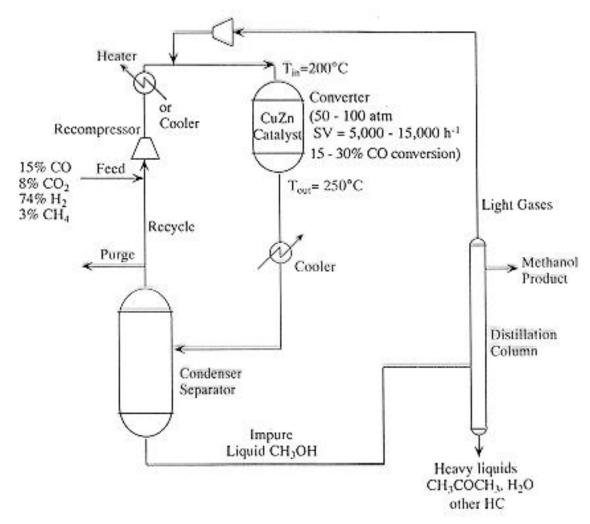
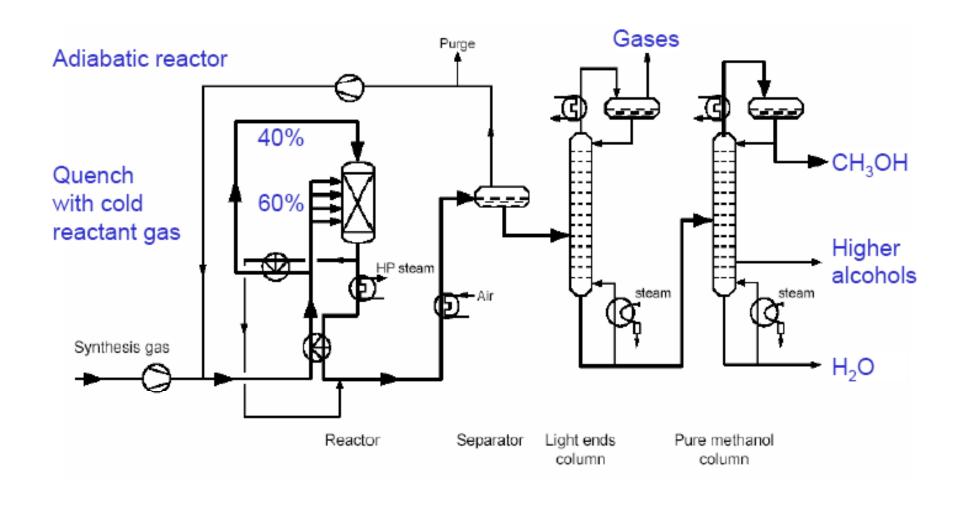


Figure 6.15 Flow sheet of typical low pressure methanol plant based on the steam reforming of natural gas.

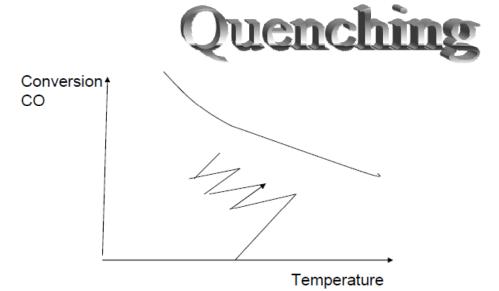
ICI-low pressure methanol process





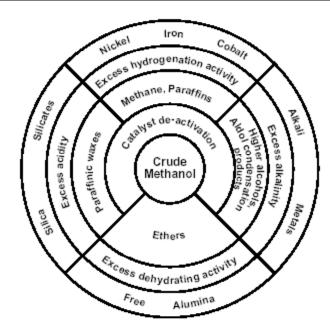
Temperature

Maximum reaction rate curve

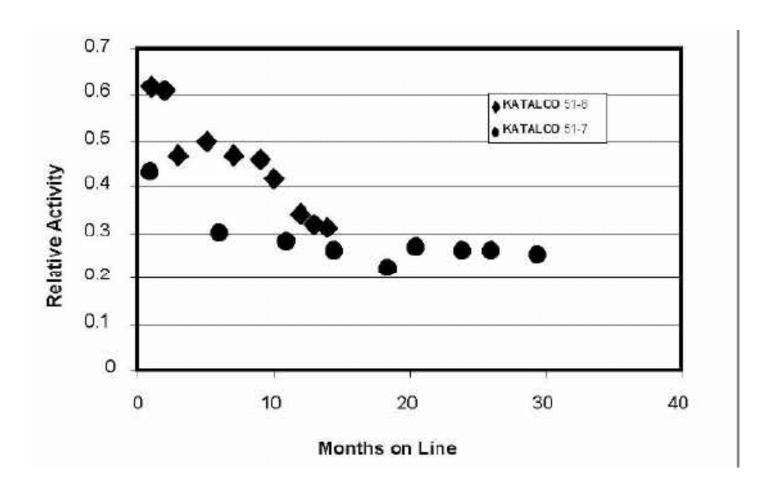


Catalysts

	Physical Properties (Typical)	Chemical Composition (Typical)		
	KATALCO 51-8			
Form	Cylindrical pellet	CuO:	64 wt%	
Diameter	5.4 mm	Al ₂ O ₃ :	10 wt%	
Length	5.2 mm	ZnO:	24 wt%	
Bulk Density	1250 kg/m ³	MgO:	2 wt%	
Crush Strength	80 kg _f			
(axial)				



Catalyst Activity

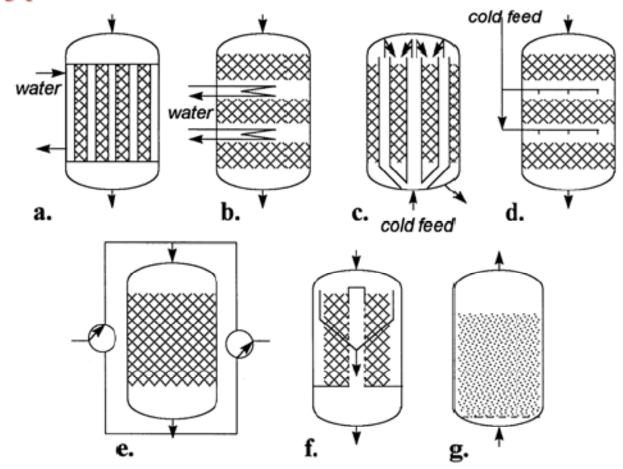


Operation policy: increase pressure, not T

Crude methanol analysis from a modern converter

Impurity (ppm w/w)	Start of run	Middle of run	End of run	
		·		
Higher alcohols				
Ethanol	110	200	265	
N-Propanol	35	60	80	
Iso-Propanol	20	30	45	
N-Butanol	10	15	20	
Iso-Butanol	30	60	80	
Sec-Butanol	10	20	35	
Hydrocarbons				
N-Petane	<2	<2	<2	
N-Hexane	<2	<2	<2	
N-Heptane	<2	<2	<2	
N-Octane	<2	<5	5	
N-Nonane	<5	<5	5	
N-Decane	<5	<5	5	

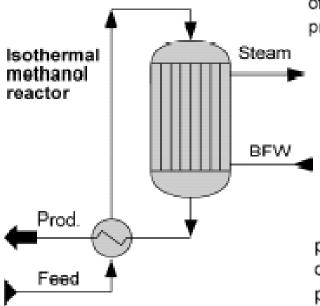
Types of reactors used for efficient cooling



- (a) Cooling with water bath; (b) cooling with water coils; (c) cooling with cold feed;
- (d) feed gas quench; (e) feed-effluent heat exchange by periodic flow reversal;
- (f) lateral flow; (g) fluidised bed.

Reactor: Isotherma

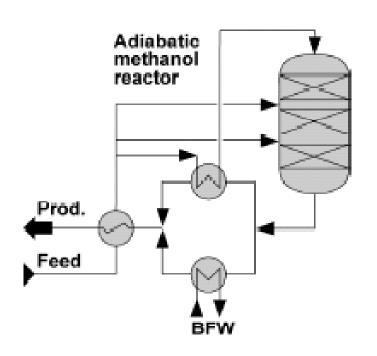
Uhde's isothermal reactor is a tubular reactor with a copper catalyst contained in vertical tubes and boiling water on the shell side. The methanol reaction heat is removed by partial evaporation of the boiler feed water, thus generating 1 metric ton of medium-pressure steam per 1.4 metric tons of methanol.



The advantages of this reactor type are: low byproduct formation due to almost isothermal reaction conditions, high reaction heat recovery, and easy temperature control by regulating steam pressure.

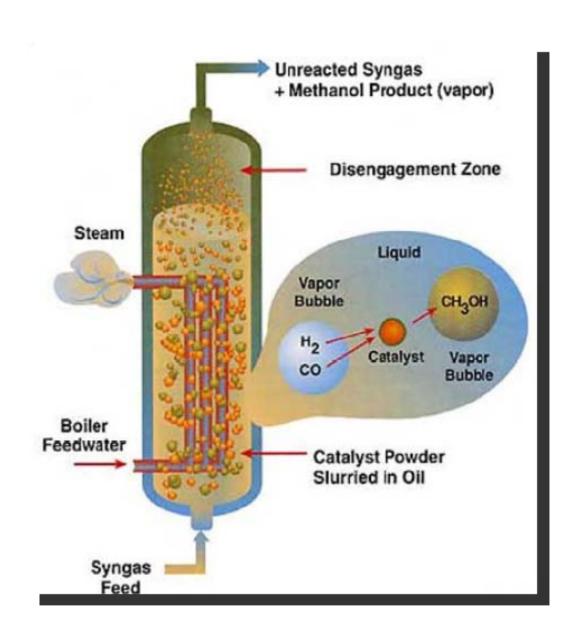
To avoid the build-up of inert components in the loop, a purge is withdrawn from the recycle gas and used as fuel for the reformer.

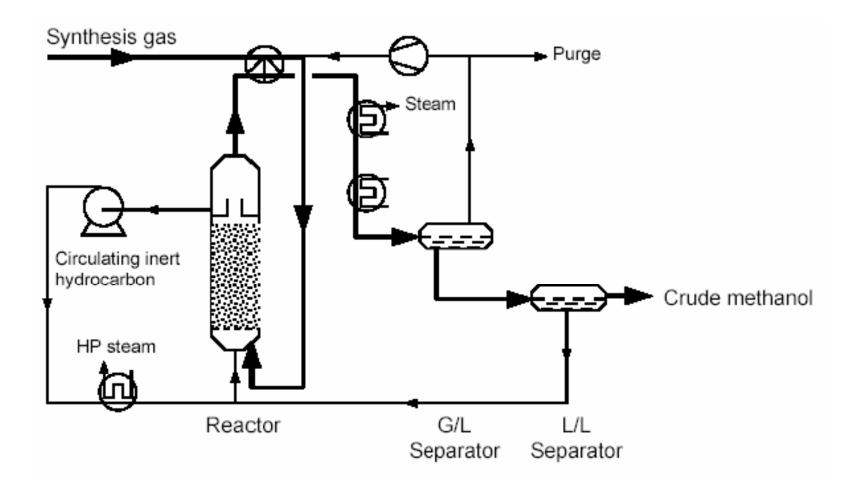
Reactor: adiabatic

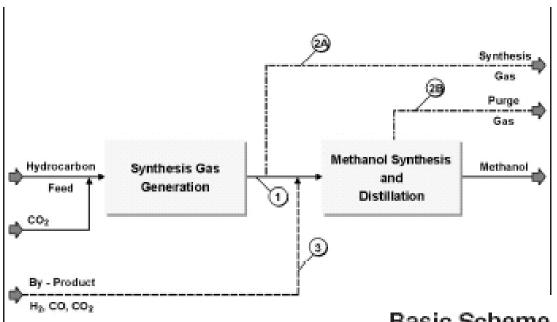


The axial radial multi-bed adiabatic quench is a low cost reactor concept. It is normally used for plants which require no steam in synthesis units, due to the fact, that surplus steam is produced during syngas generation (for instance steam reforming). Uhde can offer the ARC (Axial Radial Concept) technology licensed by Methanol Casale, Switzerland.

Methanol synthesis slurry process





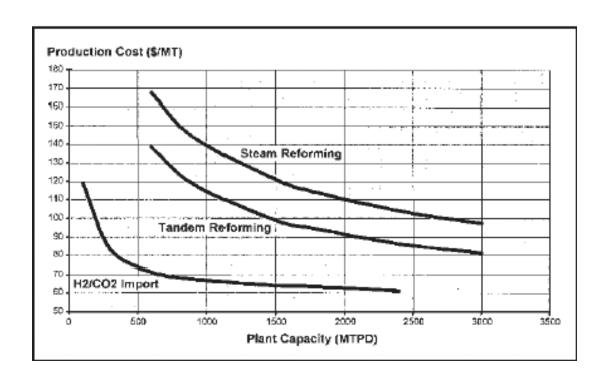


Basic Scheme 1: Routes producing syngas dedicated solely to methanol production

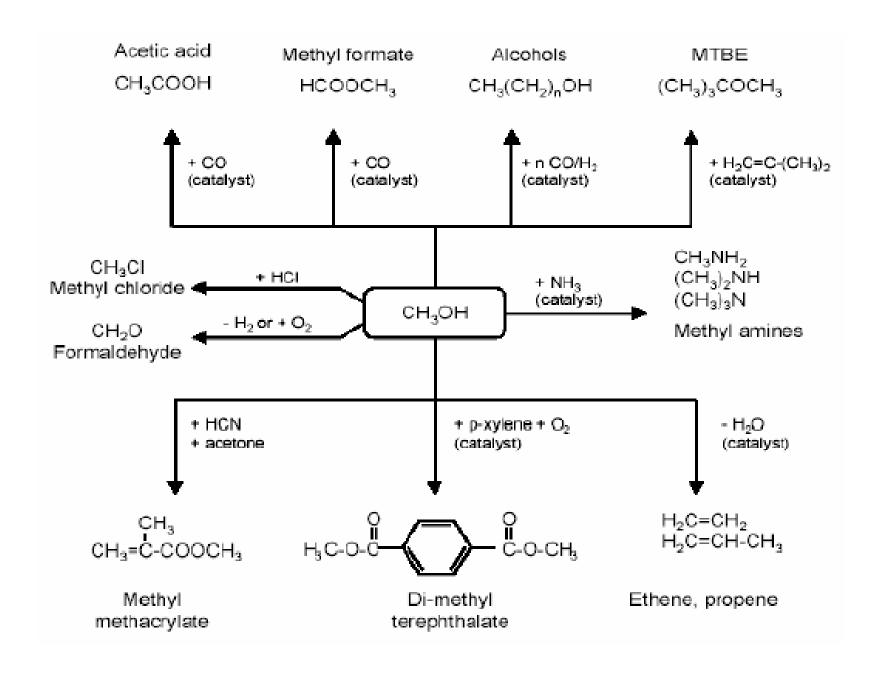
Basic Scheme 2: Routes producing syngas for methanol production as well as syngas and/or other by-products for other consumers in one train

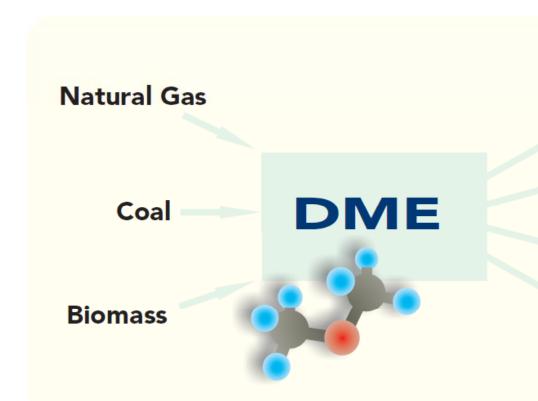
Basic Scheme 3: Routes importing methanol syngas from by-product gases available from already existing sources

Tandem



Methanol as base chemical







Diesel Alternative



LPG



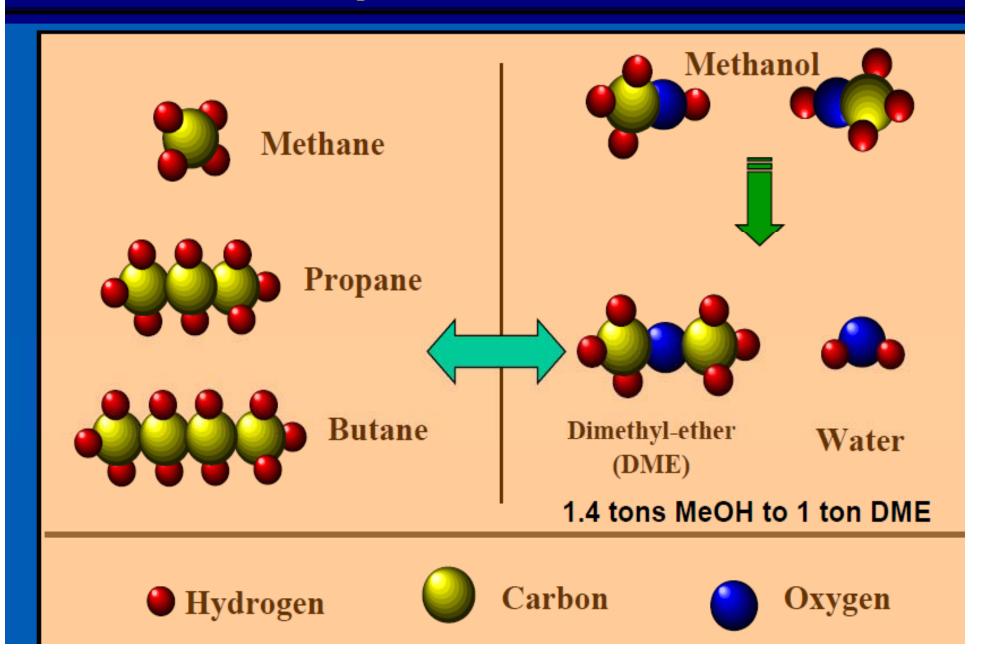
Power Production



Chemical Intermediate



DME – a simple molecule



Combustion & Fuel Injection Relevant Properties of DME and Diesel

	DME	Diesel
Chemical Structure	CH ₃ -O-CH ₃	C ₁₅ H ₂₈
Liquid Density @ 40°C [kg/m³]	634	840
Lower Calorific Value [MJ/kg]	28.4	42.7
Cetane No.	~65	40-50
Viscosity [Cst]	<0.2	~3
Boiling Point @ atm. Press. [°C]	-25	180-370

DME as Diesel Alternative

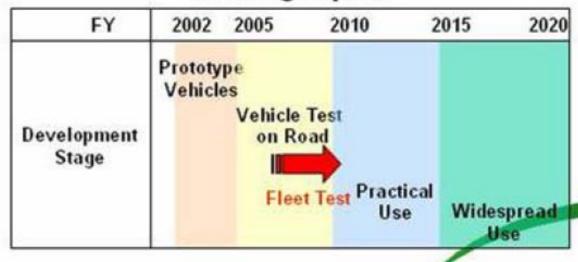
"DME is our preferred long term fuel, and under evaluation." Volvo Group (2005)

- Performs in conventional diesel engines with modified fuel injection system
 - High cetane
 - Quiet combustion
- Clean-burning: substantially lower emissions than diesel
 - Completely SOOTLESS (No smoke or particulates)
 - 100% SOx reduction
- Challenges
 - Poor compatibility with polymers: fluorine based polymers can be used
 - · Lower lubricity requires lubricating agent
 - · Lower viscosity can cause leakage
 - Requires LPG-like distribution system
 - Government regulations





Strategic plan



Fleet test plan in Japan

Periodical vehicle emission test in NTSEL



DME manufacturing / supply station



DME tank truck







National Project of City Bus Fuelled with DME





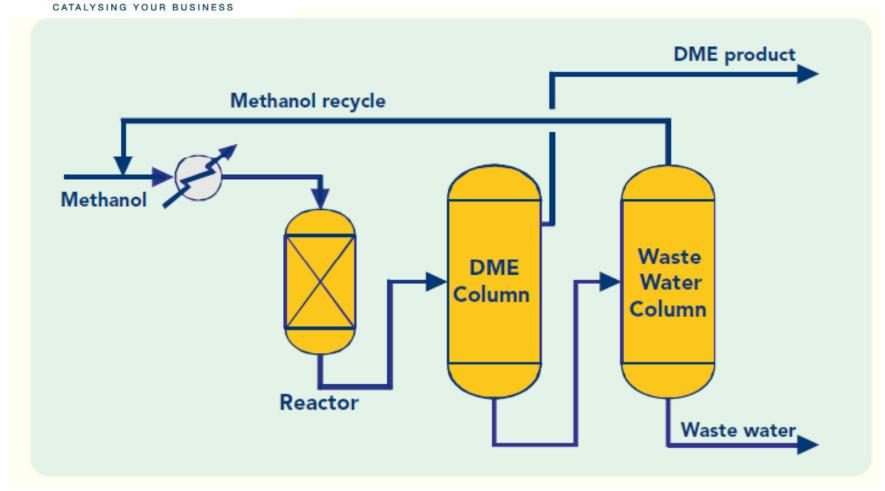


DME in Iran

World's First Large-Scale DME Plant

- Production capacity: 800,000 T/yr
- Owner: Zagros Petrochemical Co.
- Location: Bandar Assalouyeh/ Pars Special Economic/Energy Zone
- Licensor: NPC-RT and Haldor Topsoe AS
- Feed: ASTM Grade AA Methanol
- Technology: methanol dehydration, fixed-bed reactor
- Product purity (wt%) above 99%
- Primary market: LPG substitute in Iran and Region
- Current Project Status:
 - •EPC company selected
 - •First production in 2008



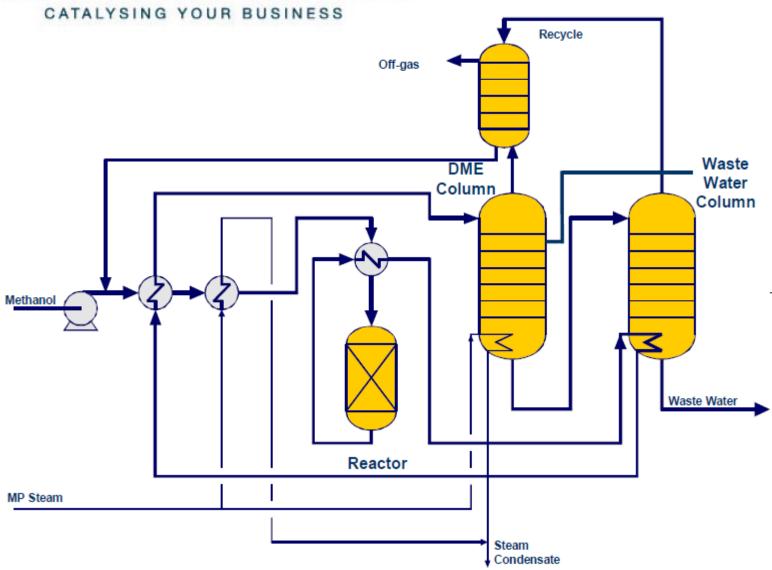


$$2 \text{ CH}_3\text{OH} \rightarrow \text{CH}_3\text{-O-CH}_3 + \text{H}_2\text{O}$$
 $-\Delta \text{H}_{298} = 23.4 \text{ kJ/mol}$

Operative conditions for DME

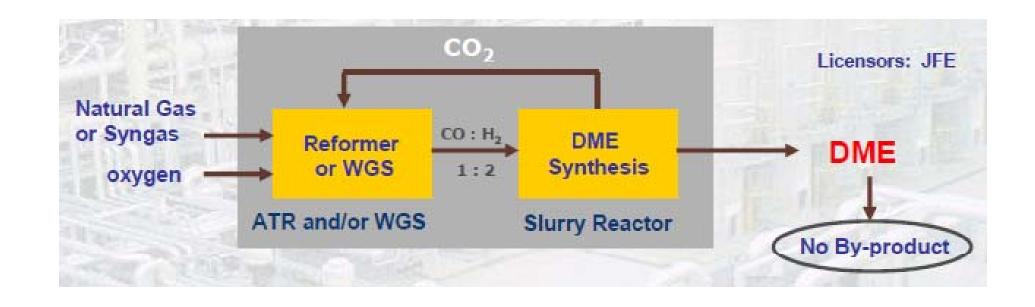
- Feed methanol is fed to a DME reactor after vaporization.
- The synthesis pressure is 1.0 2.0 MPa.
- The inlet temperature is 220 250 °C and the outlet is 300 - 350 °C.
- Methanol one pass conversion to DME is 70 – 85 % in the reactor.





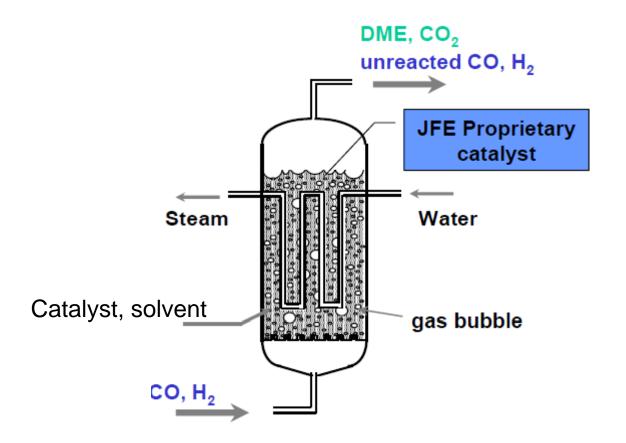


alumina



100 MTPD demo unit

- SU December 2003
- 346 day runtime
- 19,520 ton DME



Pro

- Good temperature control
- No diffusion limitation
- Rapid load response
- In-line catalyst replacement

Con

- Complicated reactor layout (3 phases)
- Small catalyst loading fraction
- Catalyst attrition & distribution

Biorefinery R&D Focus: Remove Technical Barriers

